# In-depth Study on RTT-HC-MTT Relationship for Passenger Demand beyond Elevator Contract Capacity by Simulation 

Albert T. So ${ }^{1}$ and Lutfi Al-Sharif ${ }^{2}$<br>${ }^{1}$ Faculty of Arts, Science \& Technology, University of Northampton, England ${ }^{2}$ Al Hussein Technical University, Jordan


#### Abstract

The traditional elevator system design practice is to calculate the round trip time (RTT) and associated parameters of pure incoming traffic during uppeak, followed by real-time computer simulation. Recent studies indicated that the normal traffic is much more complicated, consisting of a mixture of incoming, outgoing and interfloor patterns. The Universal RTT, under such complicated traffic patterns, was analytically developed eight years ago based on the concept of an appropriate origin-destination matrix describing the passenger transit probability and verified by Monte Carlo simulation. That model is based on the assumption that the total number of passengers demanding service within one round trip is limited to the elevator contract capacity, which is in line with the traditional uppeak incoming RTT formula. The idea of extending the consideration beyond the contract capacity was initiated two years ago. In this article, an in-depth study on such consideration is carried out so that the performance such as RTT, handling capacity (HC) and mean transit time (MTT) etc. under different traffic patterns is evaluated and analyzed with the help of Monte Carlo simulation. This article may help designers optimally size an elevator system during the RTT calculation stage without oversizing it if the prevalent traffic patterns of the building are known.


Elevator system designers, according to ISO 8100:32:2020 and CIBSE Guide D: 2020, are recommended to carry out calculation of the RTT and related parameters before any real-time computer simulation. This practice has been accepted by the elevator industry for a long time. However, conventional RTT evaluation normally considers a pure incoming traffic during uppeak. The Universal RTT calculation method developed in 2014-15 [1-3] extended RTT evaluation to consider different traffic patterns, including intra-entrance, incoming, outgoing and interfloor etc. But the total number of passengers being handled within one round trip was limited to the rated capacity of the elevator car, which could from time to time oversize the system design. The consideration to extend it beyond the rated capacity was initiated. This article provides an in-depth study on such extension by considering different traffic patterns with the help of Monte Carlo simulation, aiming at a more optimal system design by RTT calculation.

Keywords: Elevators, Universal round trip time, Handling capacity, Transit time, Contract capacity, Monte Carlo simulation.

## NOMENCLATURE

| Symbol | Full Name | Symbol | Full Name | Symbol | Full Name |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $P$ | total number of passengers at all floors demanding service within one round trip | CC* | contract capacity of the elevator car $=$ maximum number of passengers accommodated simultaneously | RTT | round trip time |
| $t_{v}$ | single floor jump time of the elevator under rated speed | $d_{f}$ | floor height | $v$ | rated speed of the elevator |
| $t$ (1) | single floor jump time of the elevator including acceleration and deceleration only | $t_{0}$ | door opening time | $t_{c}$ | door closing time |
| $t_{p}$ | average passenger transfer time | tpre | door pre-opening time | $t_{s d}$ | start delay time |
| H | average highest reversal floor under a pure 1-floor incoming traffic condition | $S$ | average number of stops under a pure 1-floor incoming traffic condition | UPPINT | average duration of interval under a pure 1- floor incoming traffic condition |
| $U_{i}$ | population of the $i$ th floor, $1 \leq i$ $\leq N$ | $U$ | total population of the whole building | ATT | average transit time of a passenger under a pure 1-floor incoming traffic condition |
| AWT | average waiting time of a passenger under a pure 1-floor incoming traffic condition | ic | ratio of incoming traffic demand in percent | og | ratio of outgoing traffic demand in percent |
| if | ratio of interfloor traffic demand in percent | ie | ratio of traffic demand within the entrance/exit floor stack in percent, assumed zero in this paper | HC | handling capacity conventionally measured in \% of total population, but in this article, passengers/round trip |
| B | number of floors of the entrance/exit floor stack | Y | number of floors of the occupant floor stack | $N$ | total number of floors of the building $=B+Y$ in this paper |
| $L$ | number of elevators serving the building |  |  | PTPV | passenger transition probability vector representing the probability of a passenger entering or leaving each floor |
| PDFOD | probability density function origin-destination which is a matrix representing the probability of passengers going from the $i$ th floor to the $j$ th floor | CDFOD | cumulative distribution function origin-destination which is the sum of probabilities of PDF OD from element $(1,1)$ to element $(i, j)$ | $\begin{aligned} & P U P, \\ & P D N \end{aligned}$ | number of passengers in the upjourney of the round trip, number of passengers in the down-journey of the round trip |
| MTT | mean transit time which is the weighted average between ATTUP and ATTDN by the $P U P$ and $P D N$ respectively | ATTUP | average transit time a passenger takes during the up journey within a round trip | ATTDN | average transit time a passenger takes during the down-journey within a round trip |

* For a formal definition of contract capacity which should be better given in terms of mass vs platform occupancy, one could refer to [4] and [5] (Section 3.7). However, in this simulation study, $C C$ only refers to the maximum number of passengers that the simulated car can accommodate to facilitate the computation of $H C$ which is measured in terms of the number of passengers being handled.


## 1 INTRODUCTION

Traditionally, the computation of the uppeak round trip time ( $R T T$ ) is the starting point of each elevator design project and the target is in-coming traffic only. It means that all passengers are assumed to enter the building at the main terminal, usually the ground floor, from the street although some are from the parking floors either above the main terminal or at the basement. This situation usually happens in the morning, say around 8:00 to $8: 30 \mathrm{am}$, at common office buildings when the whole building is rather vacant, and the rush hour just begins while occupants wait for elevator services at the lobby of the main terminal.

When one elevator car arrives at the main terminal, $P$ (number of passengers demanding service within one round trip) $\leq C C$ (the contract capacity of the elevator car) passengers enter the car, and they make car calls for their destination floors. Here, $P$ is equivalent to the total demand of one round trip. For pure incoming traffic, $P$ cannot be larger than $C C$ because almost all passengers enter the car on the same floor, i.e. the main terminal. However, when interfloor and outgoing traffic modes are also considered, $P$ could be larger than $C C$, which is the main theme of this series of studies because not all $P$ passengers enter the elevator car at the entrance floors. This phenomenon when $P$ $>C C$ is only valid under one or both conditions, i.e.
i) the existence of multiple entrance floors in a building, and
ii) mixed traffic conditions.

Perhaps a simple example could explain the former case. If one or two out of the $C C$ passengers entering the elevator car at the ground floor want to pick up their cars on the parking floors, i.e. still considered as entrance floors, they may leave the elevator car at the parking floors where one or more passengers waiting for services at these floors could enter the car and fill up the vacancies. Under this condition, $P>C C$ within that particular round trip.

As mentioned above, under a pure incoming traffic condition and classically, $P$ obviously cannot go beyond $C C$. At the same time, $S(\leq P \wedge \leq N)$ number of stops during the subsequent up-journey is made until the elevator car reaches the highest reversal floor, $H \leq N$ (which is the total number of floors served by the elevator bank above the main terminal). Since both $S$ and $H$ are statistical figures, they are normally non-integers by calculation but for each single round trip, both must be integers. At the $S$ th stop (excluding the first stop at the main terminal) and at the $H$ th floor, the elevator car becomes vacant, which will then make an express down-trip back to the main terminal. This completes a standard round trip with a well-defined $R T T$. Equation (1) is the standard equation used to estimate such RTT, based on Chapter 3 of [5].
$R T T=2 H \frac{d_{f}}{v}+(S+1)\left(t_{c}+t_{s d}+t_{f}(1)+t_{o}-t_{p r e}-\frac{d_{f}}{v}\right)+2 P t_{p} \quad$ where
$H=$ average highest reversal floor; $d_{f}=$ average interfloor height;
$v=$ rated speed; $S=$ average number of up-stops; $t_{c}=$ door closing time;
$t_{s d}=$ start delay time; $t_{f}(1)=$ single floor flight time; $t_{o}=$ door opening time;
$t_{\text {pre }}=$ pre-door opening time; $P=$ average number of passengers inside the elevator;
$t_{p}=$ average single passenger transfer time (entry or exit).

Under a general case where the floor population density is assumed non-uniform, $S$ and $H$ can be estimated by equation set (2) according to [6] (pp. 140-141). Here, $U_{i}$ is the population of the $i$ th floor and $U$ the total population of the whole building under consideration. Actually, these two equations are also applicable to uniform population distribution as a special case by making all $U_{i}=U / N$. For equations (1) and (2) to be applicable, several assumptions have to be made.
i) Floor height is uniform and constant.
ii) Half the floor is used for acceleration and half for deceleration. In other words, a one-floor jump consists of acceleration and deceleration only.
iii) Passenger arrival rate is constant.
iv) Door opening and closing times must strictly follow the assigned values; no delay by any passenger is allowed.

Of course, suitable adjustments need to be made for them to be practical in the real world. However, for the purpose of traffic analysis and design by calculation, such simplification can reduce the burden on the calculation procedures, even when the Monte Carlo simulation is carried out. This is the format adopted throughout this article.
$S=N\left(1-\frac{1}{N} \sum_{i=1}^{N}\left(1-\frac{U_{i}}{U}\right)^{P}\right)$
$H=N-\sum_{j=1}^{N-1}\left(\sum_{i=1}^{j} \frac{U_{i}}{U}\right)^{P}$
where $U=\sum_{i=1}^{N} U_{i}$

Once the $R T T$ has been estimated, the next step is to estimate the uppeak interval, UPPINT, the handling capacity, $H C$ (conventionally represented in percent of total population of the building, but in this paper, it refers to number of passengers that can be handled by one elevator within one round trip) of a group of $L$ elevators, the average waiting time [6] (page 120), $A W T$, and the average transit time [7], ATT, of passengers under such uppeak traffic condition by using equation set (3). The relationship between $A W T$ and $U P P I N T$ in equation set (3) may not be always reliable, in particular, when the demand is getting higher [8]. After all, on page 120 of [6], it is stated that equation (6.1) is just approximate.

$$
\begin{align*}
& \text { UPPINT }=\frac{R T T}{L} ; H C=\frac{300 L P}{R T T} \\
& \begin{aligned}
A W T & =\left[0.4+\left(1.8 \frac{P}{C C}-0.77\right)^{2}\right] \text { UPPINT }
\end{aligned} \text { for } 50 \% \leq \frac{P}{C C} \leq 80 \%  \tag{3}\\
& A T T
\end{aligned} \begin{aligned}
2 S & \frac{S+1}{2 S} H t_{v}+\frac{S+1}{2}\left(T-t_{v}\right)+P t_{p} \\
& \approx 0.5 H t_{v}+0.5 S\left(T-t_{v}\right)+1.5 P t_{p} \quad \text { quoted in CIBSE Guide D } 2015
\end{align*}
$$

In practice, under very heavy traffic, $P$ is very close to $C C$ and then, the $A W T$ could be approaching a very large value, as shown by Figure 6.1 [6] (page 121). According to the second equation on the first row of equation set (3), based on the required handling capacity of the building during a 5-minute uppeak period, the total number of elevators of the system, $L$, is determined. Of course, $P \leq C C$. At this point, the brief design has been completed; the next step recommended by the [9] is to carry out a real-time computer simulation to optimize different configurations.

This traditional process of traffic analysis by calculation has the following characteristics:
i) There are incoming passengers only who normally enter the building at the main terminal on the ground floor.
ii) A round trip normally begins at the main terminal and ends at the main terminal, which may not be the case if there are parking floors above or below the main terminal.
iii) The main issue is that only $P \leq C C$ number of passengers is considered within one round trip. Suppose the whole building is served by one elevator only and if $P>C C$, the remaining ( $P$ $C C$ ) passengers have to wait for service during the next round trip of the elevator.

For (i), it has already been confirmed [10-13] that uppeak traffic is no longer the dominant traffic pattern in a modern office building. Furthermore, the lunch peak mainly consisting of mixed traffic patterns may be even worse, which is considered the main challenge to an elevator system [14-16]. It is customary nowadays to quantitatively describe the prevailing traffic in a modern high-rise building at any time as a mixture of simultaneous incoming, outgoing and interfloor traffic demands [3].

For (ii), a new definition of a typical round trip using the ring concept of a virtual round trip was proposed [17, 2], the detailed discussion of which is beyond the scope of this article. The concept of a virtual interval was first suggested by [17] where the round trip time is more generally defined as the time from the moment the elevator car starts up to the next time it starts up after two reversals. The concept was further strengthened by [2] with the introduction of the "sense of reversal". Having said that, this new definition has been adopted in the simulation processes discussed in this article.

For (iii), when pure incoming traffic is considered, it is obvious that the elevator car is loaded with $P$ ( $\leq C C$ ) number of passengers at the main terminal and some parking floors. Only these $P$ passengers are served during that particular round trip. However, when outgoing and interfloor, in particular, passengers exist within that round trip, the total number of passengers served by the elevator car could be many more than $C C$. For example, $C C$ number of passengers enters the elevator car at the ground floor and destinations of $(C C-1)$ passengers are identical, say $5 / \mathrm{F}$ which is an occupant floor. The remaining passenger's destination is the top floor, the $N$ th floor. When the car reaches 5/F, all (CC 1) passengers leave and the car becomes almost vacant, except one passenger staying behind. Under this situation, the elevator can flexibly serve up-going passengers from 5/F until the ( $N-1$ )th floor whenever there are some vacancies inside. On the $N$ th floor, the car becomes vacant again and it can flexibly serve down-going passengers from the $N$ th floor until the floor above the main terminal. Under this consideration, the elevator car has actually served many more than $C C$ passengers during that particular round trip. The simulations that follow have shown that although the RTT may be very much lengthened, the $H C$ can be significantly increased as well. So, if only $P \leq C C$ number of passengers can be served within one round trip, as in the traditional way of calculation, the handling capacity may be seriously underestimated. Then, $L$, the total number of elevators of the system, may be seriously over estimated or the system design is oversized.

The idea of estimating the $R T T$ of a typical round trip under the situation when $P>C C$ was first proposed and studied by So [18]. In the following sections, the methodology is briefly described again for the sake of completeness. Details of the mathematics can be found in [18]. Results of detailed performance study under different traffic patterns by Monte Carlo simulation will then be discussed as the main contribution of this article.

## 2 THE ORIGIN-DESTINATION MATRIX

There are two types of floors within a building, namely the entrance/exit floors and the occupant floors. At entrance/exit floors, building occupants can either enter or leave the building. Entrance floors need not be contiguous. By occupant floors, building occupants stay there to work or stay. At the same time, occupant floors need not be contiguous. But normally, they are contiguous in practice. Then, four types of traffic are typical, namely
i) Inter-entrance/exit floor traffic means passengers travel within the entrance/exit floor zone. For example, a passenger enters the elevator at the ground floor and leaves it at the 3rd parking floor to pick up the car etc. The percentage of occurrence of such traffic is termed $i e \%$ which is usually assumed zero.
ii) Incoming traffic means passengers enter the building at the entrance/exit floors with their destinations at the occupant floors. This is the most conventional type of traffic considered in RTT analysis, which usually happens during the uppeak. The percentage of occurrence is termed $i c \%$. Such $i c \%$ may further be divided and applied to different entrance floors. Usually, the proportion with the main terminal is higher.
iii) Outgoing traffic means passengers get into the elevator from occupant floors but leave the building at entrance/exit floors. This usually happens during the down peak. The percentage of occurrence is termed $o g \%$.
iv) Finally, passengers can travel between occupant floors, called interfloor traffic, termed $i f \%$.

It should be noted that $i e+i c+o g+i f=100 \%$. A typical example of the lunch time period is provided in Chapter 4 of [5] where the total 5-minute demand accounts for $13 \%$ of the overall building population with a mixture of $0 \%$ inter-entrance, $45 \%$ incoming, $45 \%$ outgoing and $10 \%$ interfloor. So, RTT calculation must consider a mixture of these three common types of traffic.

To study the universal $R T T$, either by calculation or by simulation, the first step is to create a passenger transition probability vector (PTPV). From this vector, the probability density function origindestination (PDFOD) matrix can be produced [1-3, 16]. From PDFOD, the cumulative distribution frequency origin-destination matrix, CDFOD can be produced.

A typical building under study consists of $B$ number of floors in the entrance/exit stack (including the main terminal at the bottom of the stack) and $Y$ number of floors in the occupant stack, i.e. total number of floors served by the elevator in this building is equal to $N=B+Y$. The first floor is the main terminal at the ground floor, which is the lowest floor. This configuration, for the sake of computational convenience, is a bit different from that in the conventional $R T T$ formula where the building has $(N+1)$ floors. Here, the 1st floor is the main terminal on street level, 2 nd floor to the $B$ th floor being car parking floors. $(B+1)$ th to $[(B+Y)$ th $=N$ th $]$ are occupant floors. This assumption applies to most modern office buildings without loss of generality.
$\mathbf{P T P V}$ is an $N$ x 1 vector. $\mathbf{P T P V}(1)$ to $\mathbf{P T P V}(B)$ represent the probability of arrival of a passenger entering or leaving a particular floor within the entrance/exit floor stack, i.e. $P_{a r r}(1), P_{a r r}(2), \ldots, P_{a r r}(B)$.

As stated before, more passengers enter and leave the building via the main terminal; hence PTPV (1) $=P_{\operatorname{arr}}(1)$ is relatively larger, say $60 \%$ or more, while the remaining elements share the remaining $40 \%$ or less because sum $\mathbf{P T P V}(1)+\ldots+\mathbf{P T P V}(B)$ must be equal to unity. $\mathbf{P T P V}(B+1)$ represents the relative population density of the lowest floor of the occupant floor stack, which is equal to $U(B+1) / U$ and PTPV $(B+Y)$ represents the relative population density of the highest floor of the occupant floor stack, which is $U(B+Y) / U$, others similarly defined. Again, $\mathbf{P T P V}(B+1)+\mathbf{P T P V}(B+2)+\ldots+$ PTPV $(B+Y-1)+\mathbf{P T P V}(B+Y)$ must be equal to unity.

The $\mathbf{P D F O D}=\mathbf{P T P V}{ }^{*} \mathbf{P T P V}^{\mathrm{T}}$ is an $N \mathrm{x} N$ square matrix. Each element $\operatorname{PDFOD}(i, j)$ represents the probability a passenger wants to travel from the $i$ th floor to the $j$ th floor, $i$ or $j=1, \ldots, N$. It is reasonable nobody wants to travel from the $i$ th floor to the $i$ th floor and therefore all elements $\operatorname{PDFOD}(i, i)$ must be zero. Characteristics of PDFOD are shown in equation set (4) and all elements can be categorized under four zones or regions.
$\sum_{i=1}^{B} P_{\text {arr }}(i)=1 \quad ; \quad \sum_{i=1}^{Y} \frac{U(B+i)}{U}=1$ where $U=\sum_{i=1}^{Y} U(B+i)$
For $i \neq j, \quad \operatorname{PDFOD}(i, j)$
$=\left\{\begin{array}{ccc}P_{a r r}(i) P_{\text {arr }}(j) & (1 \leq i \leq B) \wedge(1 \leq j \leq B) & \text { inter-entrance floor traffic } \\ P_{\text {arr }}(i) \frac{U(j)}{U} & (1 \leq i \leq B) \wedge(B+1 \leq j \leq B+Y) & \text { incoming traffic } \\ \frac{U(i)}{U} P_{a r r}(j) & (B+1 \leq i \leq B+Y) \wedge(1 \leq j \leq B) & \text { outgoing traffic } \\ \frac{U(i) U(j)}{U^{2}} & (B+1 \leq i \leq B+Y) \wedge(B+1 \leq j \leq B+Y) & \text { interfloor traffic }\end{array}\right\}$
$\operatorname{PDFOD}(i, i)=0$
Since passengers are rational, who do not travel from the $i$ th floor to the $i$ th floor, all $\operatorname{PDFOD}(i, i), i$ $=1, \ldots, N$ must be set to zero. Since $i e+i c+o g+i f=1$ as discussed before, every element inside the PDFOD must be normalized in accordance with equation set (5). After this normalization process, the sum of all elements within the final PDFOD becomes unity.
$\operatorname{PDFOD}(i, j) \leftarrow \frac{\operatorname{PDFOD}(i, j) \cdot i e}{\sum_{m=1}^{B} \sum_{n=1}^{B} \operatorname{PDFOD}(m, n)}(1 \leq i \leq B) \wedge(1 \leq j \leq B) \quad$ inter-entrance floors
$\operatorname{PDFOD}(i, j) \leftarrow \frac{\operatorname{PDFOD}(i, j) \cdot i c}{\sum_{m=1}^{B} \sum_{n=B+1}^{N} \operatorname{PDFOD}(m, n)} \quad(1 \leq i \leq B) \wedge(B+1 \leq j \leq N) \quad$ incoming floors
$\operatorname{PDFOD}(i, j) \leftarrow \frac{\operatorname{PDFOD}(i, j) \cdot o g}{\sum_{m=B+1}^{N} \sum_{n=1}^{B} \operatorname{PDFOD}(m, n)} \quad(B+1 \leq i \leq N) \wedge(1 \leq j \leq B) \quad$ outgoing floors
$\operatorname{PDFOD}(i, j) \leftarrow \frac{\operatorname{PDFOD}(i, j) \cdot i f}{\sum_{m=B+1}^{N} \sum_{n=B+1}^{N} \operatorname{PDFOD}(m, n)} \quad(B+1 \leq i \leq N) \wedge(B+1 \leq j \leq N) \quad$ interfloor floors
This matrix, PDFOD is extremely important in the subsequent Monte Carlo simulation.
From PDFOD, CDFOD is generated according to equation (6). This CDFOD is also an $N \mathrm{x} N$ matrix.
$\operatorname{CDFOD}(i, j)=\sum_{m=1}^{i-1} \sum_{n=1}^{N} \operatorname{PDFOD}(m, n)+\sum_{n=1}^{j} \operatorname{PDFOD}(i, n)$
To produce a particular passenger within one round trip in the Monte Carlo simulation, a random number, $0 \leq R \leq 1$, is generated while the passenger's origin floor $(i)$, and the destination floor $(j)$ can be determined based on one of the two following criteria as shown in equation set (7). For the second criterion, $j=1$.
$\operatorname{CDFOD}(i, j-1)<R \leq \operatorname{CDFOD}(i, j) \quad$ or
$\operatorname{CDFOD}(i-1, N)<R \leq \operatorname{CDFOD}(i, 1) \quad \wedge \quad j=1$
It can be seen that $\operatorname{CDFOD}(1,1)=0$ while $\operatorname{CDFOD}(N, N)=1$ while all other elements are real numbers between 0 and 1 , inclusive. To simulate one round trip, first of all, the total number of passengers, $P$, who demand service must be suggested. Since there is no more constraint, $P \leq C C$, now, not all $P$ passengers may be served within the same round trip though the demand is $P$; it really depends on the relative distribution of them. By using CDFOD, the origin and destination floors of all these $P$ passengers are determined as $P$ number of random number generations is performed.

For one particular round trip, the elevator car undergoes an up-journey, followed by a down-journey. The car always starts at the lowest floor with at least one up-going passenger, picks the passenger(s) up, stops at the highest floor to release the last up-going passenger, changes its direction, picks up the first down-going passenger at the highest floor with this passenger, and finally releases the last downgoing passenger at this passenger's destination floor. It should be noted that the highest floor during the up-journey may not be the same as the highest floor during the down-journey while the lowest floor during the up-journey may not be the same as the lowest floor during the down-journey.

The number of stops during the up-journey and the down-journey is different and their sum gives the total number of stops. However, very often, the lowest stop of an up-journey is identical to that of a down-journey, and similarly for the highest stop. Whenever there is any overlapping of either the lowest floor and/or the highest floor, one or two stops must be subtracted from the total. The total time for a round trip is the $R T T$ in this article. The round trip always starts from the lowest floor of the up-journey and ends on the same floor, as discussed before using the new definition of the ring concept of a round trip. By Monte Carlo simulation, half a million trials are conducted, and the average results are statistically used.

During a particular round trip, the exact total number of passengers that can be served is termed handling capacity, $H C$, in this article, which is equal to or less than the total demand of that round trip, $P$. This $H C$ number of passengers can be divided into two groups, those up-going and those down-going and their sum is $H C$ and $H C \leq P$. After half a million trials, the average number of upgoing passengers, $P U P$, and the average number of down-going passengers, $P D N$, can be estimated. At the lowest stop of the up-journey, certain passengers enter the car. At the next stop along the upjourney, some passengers may exit and enter the car. This process continues until the car is full. Then, the remaining passengers on the floor cannot be served anymore. A full car does not stop at any floor with waiting passengers only. The exact time spent by each passenger inside the car is recorded, called transit time, $T T$. There are up-transit and down-transit times respectively as it is assumed that no up-passenger stays inside a down-traveling car. Again, the average up-TT (ATTUP) and down-TT $(A T T D N)$ of half a million trials are used. To calculate the overall mean transit time, MTT, of half a million trials, equation (8) is used. These are parameters used for analysis in the simulation.
$M T T=\frac{P U P * A T T U P+P D N^{*} A T T D N}{(P U P+P D N)}$
As mentioned before, though $P$ is fixed, the exact $H C$ of each round trip differs because it very much depends on the distribution of these $P$ passengers of that particular round trip. This is the core subject of consideration in this article. Table 1 shows an example with some exaggeration of course. For example, $N=4$ is considered, $C C=10$ and $P=30$. The table provides a comparison between two rather extreme scenarios.

Table 1 Comparison of Extreme Scenarios that affect Handling Capacity significantly

| Scenario 1 |  | Scenario 2 |  |
| :--- | :--- | :--- | :--- |
| Number of passengers | From Floor/To Floor | Number of passengers | From Floor/To Floor |
| 10 | $1 / 2$ | 20 | $1 / 4$ |
| 10 | $2 / 3$ | 5 | $2 / 3$ |
| 10 | $3 / 4$ | 5 | $3 / 4$ |
|  |  |  |  |
| Total passengers handled $=30$ | Total passengers handled $=10$ |  |  |

In both cases, there are 30 passengers who demand service. In scenario 1 , the elevator can handle all 30 passengers $(H C=30)$ within the same round trip, while in scenario 2 , only 10 passengers ( $H C=$ 10) can be entertained. Even on the first floor, only half of the 20 waiting passengers can get into the elevator which bypasses both 2 nd and 3rd floors. Obviously, the $R T T$ of scenario 1 is certainly much longer than that of scenario 2 . Which one is more favorable very much depends on the average waiting time, $A W T$, and the average transit time, $A T T$, of passengers. In traditional traffic analysis by calculation, these scenarios are not considered because only incoming traffic during an uppeak period is considered, and therefore the overall design tends to be too ideal and over-simplified, and from time to time, the system is over-sized. In this study, the consideration is more realistic and a more practical $R T T$ is arrived at by simulation.

## 3 THE MONTE CARLO SIMULATION

The study is on a building with the main terminal at the ground floor (1st floor), two parking floors above ( $2 / \mathrm{F}$ and $3 / \mathrm{F}$ ), and then eight occupant floors ( $4 / \mathrm{F}$ to $11 / \mathrm{F}$ ), i.e. $N=11$. Floor height is assumed uniform with the following technical parameters of the elevator as shown in Table 2.

Table 2 Technical Parameters of the Elevator under study

| Parameter | Value | Parameter | Value |
| :--- | :--- | :--- | :--- |
| $C C$ | 10 passengers | $t_{v}$ | 2 s |
| $d_{f}$ | 4 m | $v$ | $2 \mathrm{~m} / \mathrm{s}$ |
| $t_{o}$ | 1 s | $t_{c}$ | 3 s |
| $t_{f}(1)$ | 4.7 s | $t_{p}$ | 1.2 s |
| $t_{p r e}$ | 0 s | $t_{s d}$ | 0 s |
| $B$ | 3 floors | $Y$ | 8 floors |
| $N$ | 11 floors |  |  |

Table 3 shows the PTPV of this building. Most passengers enter and exit the building via the first floor. The population of all occupant floors is uniform. Different ratios of ie: ic: og: if have been used and the results are discussed in the next section. Table 4(a) shows the final PDFOD matrix and Table 4(b) the CDFOD matrix.

Table 3 Passenger Transition Probability Vector for simulation (uniform population distribution on occupant floors)

| $P_{\text {arr }}(1)$ | $P_{\text {arr }}(2)$ | $P_{\text {arr }}(3)$ | $U(4) / U$ | $U(5) / U$ | $U(6) / U$ |
| :--- | :--- | :--- | :--- | :--- | :--- |
| 0.6 | 0.2 | 0.2 | 0.125 | 0.125 | 0.125 |
| $U(7) / U$ | $U(8) / U$ | $U(9) / U$ | $U(10) / U$ | $U(11) / U$ |  |
| 0.125 | 0.125 | 0.125 | 0.125 | 0.125 |  |

Table 4(a) The Probability Distribution Function Origin-Destination Matrix after normalization (uniform population distribution)

| 0.0000 | 0.0000 | 0.0000 | 0.0262 | 0.0262 | 0.0262 | 0.0262 | 0.0262 | 0.0262 | 0.0262 | 0.0262 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 0.0000 | 0.0000 | 0.0000 | 0.0087 | 0.0087 | 0.0087 | 0.0087 | 0.0087 | 0.0087 | 0.0087 | 0.0087 |
| 0.0000 | 0.0000 | 0.0000 | 0.0087 | 0.0087 | 0.0087 | 0.0087 | 0.0087 | 0.0087 | 0.0087 | 0.0087 |
| 0.0262 | 0.0087 | 0.0087 | 0.0000 | 0.0054 | 0.0054 | 0.0054 | 0.0054 | 0.0054 | 0.0054 | 0.0054 |
| 0.0262 | 0.0087 | 0.0087 | 0.0054 | 0.0000 | 0.0054 | 0.0054 | 0.0054 | 0.0054 | 0.0054 | 0.0054 |
| 0.0262 | 0.0087 | 0.0087 | 0.0054 | 0.0054 | 0.0000 | 0.0054 | 0.0054 | 0.0054 | 0.0054 | 0.0054 |
| 0.0262 | 0.0087 | 0.0087 | 0.0054 | 0.0054 | 0.0054 | 0.0000 | 0.0054 | 0.0054 | 0.0054 | 0.0054 |
| 0.0262 | 0.0087 | 0.0087 | 0.0054 | 0.0054 | 0.0054 | 0.0054 | 0.0000 | 0.0054 | 0.0054 | 0.0054 |
| 0.0262 | 0.0087 | 0.0087 | 0.0054 | 0.0054 | 0.0054 | 0.0054 | 0.0054 | 0.0000 | 0.0054 | 0.0054 |
| 0.0262 | 0.0087 | 0.0087 | 0.0054 | 0.0054 | 0.0054 | 0.0054 | 0.0054 | 0.0054 | 0.0000 | 0.0054 |
| 0.0262 | 0.0087 | 0.0087 | 0.0054 | 0.0054 | 0.0054 | 0.0054 | 0.0054 | 0.0054 | 0.0054 | 0.0000 |

## Table 4(b) The Cumulative Distribution Frequency Origin-Destination Matrix (uniform population distribution)

| 0.0000 | 0.0000 | 0.0000 | 0.0262 | 0.0525 | 0.0787 | 0.1050 | 0.1312 | 0.1575 | 0.1837 | 0.2100 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 0.2100 | 0.2100 | 0.2100 | 0.2187 | 0.2275 | 0.2362 | 0.2450 | 0.2537 | 0.2625 | 0.2712 | 0.2800 |
| 0.2800 | 0.2800 | 0.2800 | 0.2887 | 0.2975 | 0.3062 | 0.3150 | 0.3237 | 0.3325 | 0.3412 | 0.3500 |
| 0.3762 | 0.3850 | 0.3937 | 0.3937 | 0.3991 | 0.4045 | 0.4098 | 0.4152 | 0.4205 | 0.4259 | 0.4312 |
| 0.4575 | 0.4662 | 0.4750 | 0.4804 | 0.4804 | 0.4857 | 0.4911 | 0.4964 | 0.5018 | 0.5071 | 0.5125 |
| 0.5387 | 0.5475 | 0.5562 | 0.5616 | 0.5670 | 0.5670 | 0.5723 | 0.5777 | 0.5830 | 0.5884 | 0.5937 |
| 0.6200 | 0.6287 | 0.6375 | 0.6429 | 0.6482 | 0.6536 | 0.6536 | 0.6589 | 0.6643 | 0.6696 | 0.6750 |
| 0.7012 | 0.7100 | 0.7187 | 0.7241 | 0.7295 | 0.7348 | 0.7402 | 0.7402 | 0.7455 | 0.7509 | 0.7562 |
| 0.7825 | 0.7912 | 0.8000 | 0.8054 | 0.8107 | 0.8161 | 0.8214 | 0.8268 | 0.8268 | 0.8321 | 0.8375 |
| 0.8637 | 0.8725 | 0.8812 | 0.8866 | 0.8920 | 0.8973 | 0.9027 | 0.9080 | 0.9134 | 0.9134 | 0.9187 |
| 0.9450 | 0.9537 | 0.9625 | 0.9679 | 0.9732 | 0.9786 | 0.9839 | 0.9893 | 0.9946 | 1.0000 | 1.0000 |

Altogether, twelve scenarios have been studied by Monte Carlo simulation. The first four belong to the typical or normal office traffic patterns including uppeak, down peak, and two lunch peaks based on Chapter 4 of CIBSE (2020). By these four scenarios, the general performance of several
selected parameters under these regular traffic patterns could be studied. Then, eight more scenarios which behave in between those typical patterns or under extreme conditions have been studied to find out the trends in more detail. Since it is assumed that all $P$ passengers have already been waiting on different floors at the beginning of each round trip simulation, it is difficult to study their overall waiting time. Therefore, $A W T$ is not included in the simulation process discussed by this article.

The building, entrance/exit - occupant floor arrangement, all elevator static/dynamic parameters, and the population distribution on each floor remain unchanged throughout the simulation process because the target is to understand the changes in selected parameters upon the variation of $P$ of each round trip. All passenger flows between inter-entrance/exit floors are ignored because the chance of occurrence is low enough to be neglected. These twelve scenarios are shown in Table 5.

Table 5 Details of the $\mathbf{1 2}$ scenarios under simulation

| Scenario | Type | $P_{\text {arr }}(1)$ | $P_{\text {arr }}(2)$ | $P_{\text {arr }}(3)$ | ic | og | if |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Uppeak | 0.6 | 0.2 | 0.2 | 0.85 | 0.10 | 0.05 |
| 2 | Down peak | 0.6 | 0.2 | 0.2 | 0.10 | 0.85 | 0.05 |
| 3 | Lunch 1 | 0.6 | 0.2 | 0.2 | 0.45 | 0.45 | 0.10 |
| 4 | Lunch 2 | 0.6 | 0.2 | 0.2 | 0.40 | 0.40 | 0.20 |
| 5 | Weak Uppeak with Interfloor | 0.6 | 0.2 | 0.2 | 0.55 | 0.15 | 0.30 |
| 6 | Weak Down peak with Interfloor | 0.6 | 0.2 | 0.2 | 0.15 | 0.55 | 0.30 |
| 7 | Uppeak with Interfloor | 0.6 | 0.2 | 0.2 | 0.70 | 0.00 | 0.30 |
| 8 | Down peak with Interfloor | 0.6 | 0.2 | 0.2 | 0.00 | 0.70 | 0.30 |
| 9 | Mixed | 0.6 | 0.2 | 0.2 | 0.35 | 0.35 | 0.30 |
| 10 | Pure Incoming | 0.6 | 0.2 | 0.2 | 1.00 | 0.00 | 0.00 |
| 11 | Pure Outgoing | 0.6 | 0.2 | 0.2 | 0.00 | 1.00 | 0.00 |
| 12 | Pure Interfloor | 0.6 | 0.2 | 0.2 | 0.00 | 0.00 | 1.00 |

The raw results after 500,000 trials of random passenger generation and simulation are shown in the following tables. Those (a)'s are raw data while (b)'s are processed data.

Table 6(a) $i e=0.00 ; i c=0.85 ; ~ o g=0.10 ; i f=0.05$ Uppeak Scenario 1

| \# of passengers demanding <br> service around the building | 10 <br> $(C C)$ | 12 <br> $(1.2 C C)$ | 16 <br> $(1.6 ~ C C)$ | 20 <br> $(2 C C)$ | 30 <br> $(3 C C)$ | 40 <br> $(4 C C)$ |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| \# of up-stops | 8.262 | 8.564 | 8.009 | 7.496 | 7.201 | 7.270 |
| \# of down-stops | 2.211 | 2.576 | 3.273 | 3.896 | 5.220 | 6.272 |
| Highest floor reached | 10.700 | 10.762 | 10.795 | 10.816 | 10.861 | 10.896 |
| Lowest floor reached | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 |
| \# of up-passengers | 8.7 | 9.9 | 10.4 | 10.5 | 10.7 | 10.9 |
| \# of down-passengers | 1.3 | 1.5 | 2.0 | 2.5 | 3.8 | 5.0 |
| \% of up-coincidental floors | 0.156 | 0.187 | 0.240 | 0.287 | 0.386 | 0.466 |
| \% of down-coincidental floors | 0.460 | 0.524 | 0.629 | 0.711 | 0.844 | 0.916 |
| Round trip time (s) | 128.837 | 136.281 | 138.619 | 139.999 | 149.043 | 159.192 |
| Average up-transit time (s) | 52.294 | 54.951 | 53.492 | 51.244 | 49.467 | 49.411 |
| Average down-transit time $(\mathrm{s})$ | 17.232 | 19.353 | 23.059 | 26.086 | 32.149 | 36.968 |

Table 6(b) $i e=0.00 ; i c=0.85 ; ~ o g=0.10 ; i f=0.05$ Uppeak Scenario 1

| $P$ | $R T T$ | \% increase | $H C$ | \% increase | $M T T$ (up- <br> down ave) | \% increase | $H C / R T T$ |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 10 | 128.837 | 0.000 | 10.000 | 0.000 | 47.736 | 0.000 | 0.078 |
| 12 | 136.281 | 5.778 | 11.400 | 14.000 | 50.267 | 5.302 | 0.084 |
| 16 | 138.619 | 7.593 | 12.400 | 24.000 | 48.583 | 1.775 | 0.089 |
| 20 | 139.999 | 8.664 | 13.000 | 30.000 | 46.406 | -2.786 | 0.093 |
| 30 | 149.043 | 15.683 | 14.500 | 45.000 | 44.928 | -5.881 | 0.097 |
| 40 | 159.192 | 23.561 | 15.900 | 59.000 | 45.498 | -4.688 | 0.100 |

Table 7(a) $i e=0.00 ; i c=0.10 ; \boldsymbol{g}=0.85 ; i f=0: 05$ Down Peak Scenario 2

| \# of passengers demanding <br> service around the building | 10 <br> $(C C)$ | 12 <br> $(1.2 C C)$ | 16 <br> $(1.6 C C)$ | 20 <br> $(2 C C)$ | 30 <br> $(3 C C)$ | 40 <br> $(4 C C)$ |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| \# of up-stops | 2.209 | 2.577 | 3.270 | 3.896 | 5.216 | 6.272 |
| \# of down-stops | 8.263 | 8.582 | 8.098 | 7.507 | 6.486 | 5.876 |
| Highest floor reached | 10.698 | 10.786 | 10.886 | 10.937 | 10.986 | 10.996 |
| Lowest floor reached | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 |
| \# of up-passengers | 1.3 | 1.5 | 2.0 | 2.5 | 3.7 | 5.0 |
| \# of down-passengers | 8.7 | 9.9 | 10.3 | 10.4 | 10.5 | 10.5 |
| \% of up-coincidental floors | 0.157 | 0.187 | 0.247 | 0.303 | 0.427 | 0.528 |
| \% of down-coincidental floors | 0.461 | 0.523 | 0.629 | 0.710 | 0.844 | 0.916 |
| Round trip time (s) | 128.810 | 136.514 | 139.488 | 140.349 | 143.966 | 148.916 |
| Average up-transit time (s) | 17.236 | 19.370 | 23.039 | 26.070 | 32.124 | 36.967 |
| Average down-transit time (s) | 52.295 | 55.338 | 56.039 | 55.430 | 53.916 | 52.861 |

Table 7(b) $i e=0.00 ; i c=0.10 ; \boldsymbol{g}=0.85 ; i f=0: 05$ Down Peak Scenario 2

| $P$ | $R T T$ | \% increase | $H C$ | \% increase | $M T T$ (up- <br> down ave) | \% increase | $H C / R T T$ |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 10 | 128.810 | 0.000 | 10.000 | 0.000 | 47.737 | 0.000 | 0.078 |
| 12 | 136.514 | 5.981 | 11.400 | 14.000 | 50.605 | 6.008 | 0.084 |
| 16 | 139.488 | 8.290 | 12.300 | 23.000 | 50.673 | 6.150 | 0.088 |
| 20 | 140.349 | 8.958 | 12.900 | 29.000 | 49.740 | 4.195 | 0.092 |
| 30 | 143.966 | 11.766 | 14.200 | 42.000 | 48.238 | 1.048 | 0.099 |
| 40 | 148.916 | 15.609 | 15.500 | 55.000 | 47.734 | -0.007 | 0.104 |

Table 8(a) $i e=0.00 ; i c=0.45 ; \boldsymbol{g}=0.45 ; i f=0: 10$ Lunch 1 Scenario 3

| \# of passengers demanding <br> service around the building | 10 <br> $(C C)$ | 12 <br> $(1.2 C C)$ | 16 <br> $(1.6 C C)$ | 20 <br> $(2 C C)$ | 30 <br> $(3 C C)$ | 40 <br> $(4 C C)$ |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| \# of up-stops | 6.253 | 6.930 | 7.950 | 8.520 | 8.401 | 7.918 |
| \# of down-stops | 6.251 | 6.929 | 7.960 | 8.545 | 8.505 | 7.898 |
| Highest floor reached | 10.723 | 10.806 | 10.898 | 10.941 | 10.979 | 10.991 |
| Lowest floor reached | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 |
| \# of up-passengers | 5.0 | 6.0 | 7.9 | 9.5 | 11.2 | 11.7 |
| \# of down-passengers | 5.0 | 6.0 | 7.9 | 9.5 | 11.2 | 11.5 |
| \% of up-coincidental floors | 0.332 | 0.394 | 0.506 | 0.599 | 0.732 | 0.795 |
| \% of down-coincidental floors | 0.915 | 0.954 | 0.987 | 0.996 | 1.000 | 1.000 |
| Round trip time (s) | 138.317 | 151.839 | 174.228 | 188.994 | 195.315 | 189.682 |
| Average up-transit time (s) | 38.882 | 42.395 | 48.173 | 51.986 | 53.081 | 50.959 |
| Average down-transit time (s) | 38.873 | 42.392 | 48.277 | 52.425 | 56.054 | 56.065 |

Table 8(b) $i e=0.00 ; i c=0.45 ; \boldsymbol{g}=\mathbf{0 . 4 5} ; i f=0: 10$ Lunch 1 Scenario 3

| $P$ | $R T T$ | \% increase | $H C$ | \% increase | MTT (up- <br> down ave) | \% increase | $H C / R T T$ |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 10 | 138.317 | 0.000 | 10.000 | 0.000 | 38.878 | 0.000 | 0.072 |
| 12 | 151.839 | 9.776 | 12.000 | 20.000 | 42.394 | 9.044 | 0.079 |
| 16 | 174.228 | 25.963 | 15.800 | 58.000 | 48.225 | 24.043 | 0.091 |
| 20 | 188.994 | 36.638 | 19.000 | 90.000 | 52.206 | 34.282 | 0.101 |
| 30 | 195.315 | 41.208 | 22.400 | 124.000 | 54.568 | 40.358 | 0.115 |
| 40 | 189.682 | 37.136 | 23.200 | 132.000 | 53.490 | 37.586 | 0.122 |

Table 9(a) $i e=0.00 ; i c=0.40 ; o g=0.40 ; i f=0: 20$ Lunch 2 Scenario 4

| \# of passengers demanding <br> service around the building | 10 <br> $(C C)$ | 12 <br> $(1.2 C C)$ | 16 <br> $(1.6 C C)$ | 20 <br> $(2 C C)$ | 30 <br> $(3 C C)$ | 40 <br> $(4 C C)$ |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| \# of up-stops | 6.400 | 7.093 | 8.146 | 8.804 | 8.995 | 8.518 |
| \# of down-stops | 6.400 | 7.087 | 8.146 | 8.826 | 9.146 | 8.724 |
| Highest floor reached | 10.768 | 10.840 | 10.922 | 10.958 | 10.988 | 10.996 |
| Lowest floor reached | 1.001 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 |
| \# of up-passengers | 5.0 | 6.0 | 8.0 | 9.7 | 12.3 | 13.2 |
| \# of down-passengers | 5.0 | 6.0 | 8.0 | 9.7 | 12.2 | 13.0 |
| \% of up-coincidental floors | 0.359 | 0.424 | 0.544 | 0.643 | 0.791 | 0.859 |
| \% of down-coincidental floors | 0.873 | 0.926 | 0.975 | 0.992 | 0.999 | 1.000 |
| Round trip time (s) | 140.573 | 154.116 | 176.902 | 193.701 | 208.296 | 205.991 |
| Average up-transit time (s) | 37.389 | 40.715 | 46.283 | 50.301 | 53.121 | 51.434 |
| Average down-transit time (s) | 37.395 | 40.684 | 46.298 | 50.565 | 55.576 | 56.420 |

Table 9(b) $i e=0.00 ; i c=0.40 ; o g=0.40 ; i f=0: 20$ Lunch 2 Scenario 4

| $P$ | $R T T$ | \% increase | $H C$ | \% increase | MTT (up- <br> down ave) | \% increase | $H C / R T T$ |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 10 | 140.573 | 0.000 | 10.000 | 0.000 | 37.392 | 0.000 | 0.071 |
| 12 | 154.116 | 9.634 | 12.000 | 20.000 | 40.700 | 8.845 | 0.078 |
| 16 | 176.902 | 25.844 | 16.000 | 60.000 | 46.291 | 23.798 | 0.090 |
| 20 | 193.701 | 37.794 | 19.400 | 94.000 | 50.433 | 34.876 | 0.100 |
| 30 | 208.296 | 48.176 | 24.500 | 145.000 | 54.343 | 45.335 | 0.118 |
| 40 | 205.991 | 46.537 | 26.200 | 162.000 | 53.908 | 44.170 | 0.127 |

Table 10(a) $i \boldsymbol{i}=\mathbf{0 . 0 0} ; \boldsymbol{i c}=\mathbf{0 . 5 5} ; \boldsymbol{g}=\mathbf{0 . 1 5} ;$ if $=\mathbf{0}: 30$ Weak Uppeak with Interfloor Scenario 5

| \# of passengers demanding <br> service around the building | 10 <br> $(C C)$ | 12 <br> $(1.2 C C)$ | 16 <br> $(1.6 C C)$ | 20 <br> $(2 C C)$ | 30 <br> $(3 C C)$ | 40 <br> $(4 C C)$ |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| \# of up-stops | 7.717 | 8.397 | 9.154 | 9.190 | 8.488 | 8.188 |
| \# of down-stops | 4.782 | 5.373 | 6.403 | 7.252 | 8.714 | 9.516 |
| Highest floor reached | 10.806 | 10.869 | 10.933 | 10.960 | 10.984 | 10.994 |
| Lowest floor reached | 1.005 | 1.001 | 1.000 | 1.000 | 1.000 | 1.000 |
| \# of up-passengers | 6.9 | 8.3 | 10.8 | 12.2 | 13.6 | 14.6 |
| \# of down-passengers | 3.1 | 3.7 | 4.8 | 6.0 | 9.0 | 11.7 |
| \% of up-coincidental floors | 0.357 | 0.420 | 0.530 | 0.618 | 0.758 | 0.844 |
| \% of down-coincidental floors | 0.616 | 0.681 | 0.779 | 0.849 | 0.940 | 0.977 |
| Round trip time $(s)$ | 140.436 | 153.137 | 172.610 | 183.852 | 197.997 | 203.394 |


| Average up-transit time (s) | 43.407 | 47.116 | 52.148 | 53.469 | 51.063 | 49.451 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| Average down-transit time (s) | 26.702 | 28.671 | 32.334 | 35.575 | 41.995 | 46.560 |

Table 10(b) $i e=0.00 ; i c=0.55 ; ~ o g=0.15 ; ~ i f=0: 30$ Weak Uppeak with Interfloor Scenario 5

| $P$ | $R T T$ | \% increase | $H C$ | \% increase | $M T T$ (up- <br> down ave) | \% increase | $H C / R T T$ |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 10 | 140.436 | 0.000 | 10.000 | 0.000 | 38.228 | 0.000 | 0.071 |
| 12 | 153.137 | 9.044 | 12.000 | 20.000 | 41.429 | 8.372 | 0.078 |
| 16 | 172.610 | 22.910 | 15.600 | 56.000 | 46.051 | 20.464 | 0.090 |
| 20 | 183.852 | 30.915 | 18.200 | 82.000 | 47.570 | 24.436 | 0.099 |
| 30 | 197.997 | 40.987 | 22.600 | 126.000 | 47.452 | 24.127 | 0.114 |
| 40 | 203.394 | 44.830 | 26.300 | 163.000 | 48.165 | 25.992 | 0.129 |

Table 11(a) $i e=0.00 ; i c=0.15 ; g g=0.55 ; i f=0: 30$ Weak Down peak with Interfloor Scenario 6

| \# of passengers demanding <br> service around the building | 10 <br> $(C C)$ | 12 <br> $(1.2 C C)$ | 16 <br> $(1.6 C C)$ | 20 <br> $(2 C C)$ | 30 <br> $(3 C C)$ | 40 <br> $(4 C C)$ |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| \# of up-stops | 4.785 | 5.370 | 6.401 | 7.255 | 8.722 | 8.518 |
| \# of down-stops | 7.719 | 8.401 | 9.192 | 9.313 | 8.727 | 8.232 |
| Highest floor reached | 10.806 | 10.870 | 10.939 | 10.970 | 10.995 | 10.999 |
| Lowest floor reached | 1.004 | 1.001 | 1.000 | 1.000 | 1.000 | 1.000 |
| \# of up-passengers | 3.1 | 3.7 | 4.8 | 6.0 | 9.0 | 11.7 |
| \# of down-passengers | 6.9 | 8.3 | 10.8 | 12.2 | 13.3 | 13.7 |
| \% of up-coincidental floors | 0.358 | 0.418 | 0.532 | 0.627 | 0.799 | 0.889 |
| \% of down-coincidental floors | 0.617 | 0.681 | 0.779 | 0.850 | 0.942 | 0.977 |
| Round trip time (s) | 140.458 | 153.152 | 172.856 | 184.618 | 198.644 | 207.307 |
| Average up-transit time (s) | 26.742 | 28.681 | 32.303 | 35.584 | 42.009 | 46.539 |
| Average down-transit time (s) | 43.405 | 47.129 | 52.555 | 55.204 | 56.435 | 56.302 |

Table 11(b) $i e=0.00 ; i c=0.15 ; g g=0.55 ; i f=0: 30$ Weak Down peak with Interfloor Scenario 6

| $P$ | $R T T$ | \% increase | $H C$ | \% increase | MTT (up- <br> down ave) | \% increase | $H C / R T T$ |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 10 | 140.458 | 0.000 | 10.000 | 0.000 | 38.239 | 0.000 | 0.071 |
| 12 | 153.152 | 9.038 | 12.000 | 20.000 | 41.441 | 8.372 | 0.078 |
| 16 | 172.856 | 23.066 | 15.600 | 56.000 | 46.324 | 21.141 | 0.090 |
| 20 | 184.618 | 31.440 | 18.200 | 82.000 | 48.736 | 27.449 | 0.099 |
| 30 | 198.644 | 41.426 | 22.300 | 123.000 | 50.613 | 32.358 | 0.112 |
| 40 | 207.307 | 47.594 | 25.400 | 154.000 | 51.805 | 35.475 | 0.123 |

Table 12(a) $i e=0.00 ; i c=0.70 ; o g=0.00 ; i f=0.30$ Uppeak with Interfloor Scenario 7

| \# of passengers demanding <br> service around the building | 10 <br> $(C C)$ | 12 <br> $(1.2 C C)$ | 16 <br> $(1.6 C C)$ | 20 <br> $(2 C C)$ | 30 <br> $(3 C C)$ | 40 <br> $(4 C C)$ |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| \# of up-stops | 8.298 | 8.940 | 9.110 | 8.663 | 8.092 | 8.093 |
| \# of down-stops | 3.167 | 3.434 | 3.955 | 4.447 | 5.497 | 6.273 |
| Highest floor reached | 10.817 | 10.875 | 10.920 | 10.940 | 10.971 | 10.986 |
| Lowest floor reached | 1.005 | 1.002 | 1.000 | 1.000 | 1.000 | 1.000 |
| \# of up-passengers | 8.1 | 9.8 | 11.8 | 12.5 | 13.6 | 14.6 |
| \# of down-passengers | 1.9 | 2.1 | 2.6 | 3.1 | 4.5 | 6.0 |
| \% of up-coincidental floors | 0.340 | 0.382 | 0.453 | 0.511 | 0.641 | 0.739 |
| \% of down-coincidental floors | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| Round trip time (s) | 137.793 | 148.517 | 158.782 | 161.686 | 170.174 | 180.628 |
| Average up-transit time (s) | 47.556 | 51.611 | 54.088 | 52.611 | 49.747 | 49.110 |
| Average down-transit time (s) | 18.414 | 19.191 | 20.772 | 22.295 | 25.754 | 28.717 |

Table 12(b) $\boldsymbol{i} \boldsymbol{i}=\mathbf{0 . 0 0} ; \boldsymbol{i c}=\mathbf{0 . 7 0 ;} \boldsymbol{o g}=\mathbf{0 . 0 0} ; \boldsymbol{i f}=\mathbf{0}: \mathbf{3 0}$ Uppeak with Interfloor Scenario 7

| $P$ | $R T T$ | \% increase | $H C$ | \% increase | MTT (up- <br> down ave) | \% increase | $H C / R T T$ |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 10 | 137.793 | 0.000 | 10.000 | 0.000 | 42.019 | 0.000 | 0.073 |
| 12 | 148.517 | 7.783 | 11.900 | 19.000 | 45.890 | 9.212 | 0.080 |
| 16 | 158.782 | 15.232 | 14.400 | 44.000 | 48.073 | 14.407 | 0.091 |
| 20 | 161.686 | 17.340 | 15.600 | 56.000 | 46.587 | 10.870 | 0.096 |
| 30 | 170.174 | 23.500 | 18.100 | 81.000 | 43.782 | 4.195 | 0.106 |
| 40 | 180.628 | 31.086 | 20.600 | 106.000 | 43.170 | 2.740 | 0.114 |

Table 13(a) $\boldsymbol{i} \boldsymbol{e}=\mathbf{0 . 0 0}$; $\boldsymbol{i c}=\mathbf{0 . 0 0} ; \boldsymbol{o g}=0.70 ;$ if $=0: 30$ Down peak with Interfloor Scenario 8

| \# of passengers demanding <br> service around the building | 10 <br> $(C C)$ | 12 <br> $(1.2 C C)$ | 16 <br> $(1.6 C C)$ | 20 <br> $(2 C C)$ | 30 <br> $(3 C C)$ | 40 <br> $(4 C C)$ |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| \# of up-stops | 3.161 | 3.427 | 3.952 | 4.448 | 5.497 | 6.270 |
| \# of down-stops | 8.306 | 8.948 | 9.216 | 8.869 | 8.067 | 7.597 |
| Highest floor reached | 10.816 | 10.876 | 10.940 | 10.971 | 10.995 | 10.999 |
| Lowest floor reached | 1.005 | 1.002 | 1.000 | 1.000 | 1.000 | 1.000 |
| \# of up-passengers | 1.9 | 2.1 | 2.6 | 3.1 | 4.5 | 6.0 |
| \# of down-passengers | 8.1 | 9.8 | 11.8 | 12.4 | 12.9 | 13.2 |
| \% of up-coincidental floors | 0.338 | 0.380 | 0.457 | 0.529 | 0.675 | 0.780 |
| \% of down-coincidental floors | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| Round trip time (s) | 137.807 | 148.533 | 159.513 | 162.841 | 168.276 | 173.679 |
| Average up-transit time (s) | 18.398 | 19.180 | 20.765 | 22.300 | 25.784 | 28.719 |
| Average down-transit time (s) | 47.596 | 51.636 | 55.639 | 56.471 | 56.301 | 55.949 |

Table 13(b) $i e=0.00 ; i c=0.00 ; o g=0.70 ; i f=0: 30$ Down peak with Interfloor Scenario 8

| $P$ | $R T T$ | \% increase | $H C$ | \% increase | MTT (up- <br> down ave) | \% increase | $H C / R T T$ |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 10 | 137.807 | 0.000 | 10.000 | 0.000 | 42.048 | 0.000 | 0.073 |
| 12 | 148.533 | 7.783 | 11.900 | 19.000 | 45.908 | 9.180 | 0.080 |
| 16 | 159.513 | 15.751 | 14.400 | 44.000 | 49.342 | 17.347 | 0.090 |
| 20 | 162.841 | 18.166 | 15.500 | 55.000 | 49.637 | 18.047 | 0.095 |
| 30 | 168.276 | 22.110 | 17.400 | 74.000 | 48.409 | 15.126 | 0.103 |
| 40 | 173.679 | 26.031 | 19.200 | 92.000 | 47.440 | 12.822 | 0.111 |

Table 14(a) $\boldsymbol{i e}=\mathbf{0 . 0 0} ; \boldsymbol{i c}=\mathbf{0 . 3 5} ; \boldsymbol{g}=\mathbf{0 . 3 5} ;$ if $=\mathbf{0}: 30$ Mixed Scenario 9

| \# of passengers demanding <br> service around the building | 10 <br> $(C C)$ | 12 <br> $(1.2 C C)$ | 16 <br> $(1.6 C C)$ | 20 <br> $(2 C C)$ | 30 <br> $(3 C C)$ | 40 <br> $(4 C C)$ |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| \# of up-stops | 6.507 | 7.208 | 8.282 | 8.989 | 9.442 | 9.012 |
| \# of down-stops | 6.510 | 7.213 | 8.282 | 9.003 | 9.579 | 9.335 |
| Highest floor reached | 10.805 | 10.870 | 10.939 | 10.970 | 10.993 | 10.998 |
| Lowest floor reached | 1.005 | 1.001 | 1.000 | 1.000 | 1.000 | 1.000 |
| \# of up-passengers | 5.0 | 6.0 | 8.0 | 9.9 | 13.1 | 14.5 |
| \# of down-passengers | 5.0 | 6.0 | 8.0 | 9.9 | 13.1 | 14.3 |
| \% of up-coincidental floors | 0.386 | 0.456 | 0.581 | 0.682 | 0.835 | 0.901 |
| \% of down-coincidental floors | 0.817 | 0.884 | 0.954 | 0.982 | 0.998 | 1.000 |
| Round trip time (s) | 142.353 | 155.910 | 178.777 | 196.605 | 217.893 | 219.359 |
| Average up-transit time (s) | 35.906 | 39.012 | 44.276 | 48.317 | 52.609 | 51.766 |
| Average down-transit time (s) | 35.894 | 39.033 | 44.275 | 48.446 | 54.179 | 55.692 |

Table 14(b) $i e=0.00 ;$ ic $=0.35 ; ~ o g=0.35 ;$ if $=0: 30$ Mixed Scenario 9

| $P$ | $R T T$ | \% increase | $H C$ | \% increase | $M T T$ (up- <br> down ave) | \% increase | $H C / R T T$ |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 10 | 142.353 | 0.000 | 10.000 | 0.000 | 35.900 | 0.000 | 0.070 |
| 12 | 155.910 | 9.524 | 12.000 | 20.000 | 39.023 | 8.698 | 0.077 |
| 16 | 178.777 | 25.587 | 16.000 | 60.000 | 44.276 | 23.330 | 0.089 |
| 20 | 196.605 | 38.111 | 19.800 | 98.000 | 48.382 | 34.767 | 0.101 |
| 30 | 217.893 | 53.065 | 26.200 | 162.000 | 53.394 | 48.730 | 0.120 |
| 40 | 219.359 | 54.095 | 28.800 | 188.000 | 53.715 | 49.625 | 0.131 |

Table 15(a) $i e=0.00 ; i c=1.00 ; \boldsymbol{g}=0.00 ; i f=0: 00$ Pure Incoming Scenario 10

| \# of passengers demanding <br> service around the building | 10 <br> $(C C)$ | 12 <br> $(1.2 C C)$ | 16 <br> $(1.6 C C)$ | 20 <br> $(2 C C)$ | 30 <br> $(3 C C)$ | 40 <br> $(4 C C)$ |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| \# of up-stops | 8.680 | 8.208 | 7.391 | 7.024 | 6.896 | 6.895 |
| \# of down-stops | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| Highest floor reached | 10.670 | 10.670 | 10.669 | 10.671 | 10.668 | 10.670 |
| Lowest floor reached | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 |
| \# of up-passengers | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 |
| \# of down-passengers | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \% of up-coincidental floors | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| \% of down-coincidental floors | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| Round trip time (s) | 120.836 | 117.674 | 112.201 | 109.748 | 108.877 | 108.877 |
| Average up-transit time (s) | 56.217 | 55.060 | 51.759 | 49.974 | 49.301 | 49.291 |
| Average down-transit time $(\mathrm{s})$ | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |

Table 15(b) $\boldsymbol{i e}=\mathbf{0 . 0 0} ; \boldsymbol{i c}=\mathbf{1 . 0 0} ; \boldsymbol{g}=\mathbf{0 . 0 0} ; \boldsymbol{i f}=\mathbf{0}: 00$ Pure Incoming Scenario 10

| $P$ | $R T T$ | \% increase | $H C$ | \% increase | $M T T$ (up- <br> down ave) | \% increase | $H C / R T T$ |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 10 | 120.836 | 0.000 | 10.000 | 0.000 | 56.217 | 0.000 | 0.083 |
| 12 | 117.674 | -2.617 | 10.000 | 0.000 | 55.060 | -2.058 | 0.085 |
| 16 | 112.201 | -7.146 | 10.000 | 0.000 | 51.759 | -7.930 | 0.089 |
| 20 | 109.748 | -9.176 | 10.000 | 0.000 | 49.974 | -11.105 | 0.091 |


| 30 | 108.877 | -9.897 | 10.000 | 0.000 | 49.301 | -12.302 | 0.092 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |
| 40 | 108.977 | -9.814 | 10.000 | 0.000 | 49.291 | -12.320 | 0.092 |

Table 16(a) $\boldsymbol{i e}=\mathbf{0 . 0 0} ; \boldsymbol{i c}=\mathbf{0 . 0 0} ; \boldsymbol{g}=1.00 ;$ if=0:00 Pure Outgoing Scenario 11

| \# of passengers demanding <br> service around the building | 10 <br> $(C C)$ | 12 <br> $(1.2 C C)$ | 16 <br> $(1.6 C C)$ | 20 <br> $(2 C C)$ | 30 <br> $(3 C C)$ | 40 <br> $(4 C C)$ |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| \# of up-stops | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| \# of down-stops | 8.681 | 8.258 | 7.446 | 6.828 | 5.816 | 5.223 |
| Highest floor reached | 10.670 | 10.763 | 10.871 | 10.927 | 10.981 | 10.995 |
| Lowest floor reached | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 | 1.000 |
| \# of up-passengers | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| \# of down-passengers | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 | 10.0 |
| \% of up-coincidental floors | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| \% of down-coincidental floors | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| Round trip time (s) | 120.842 | 118.377 | 113.370 | 109.456 | 102.894 | 98.976 |
| Average up-transit time (s) | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 | 0.000 |
| Average down-transit time (s) | 56.221 | 56.260 | 55.231 | 54.250 | 52.370 | 51.158 |

Table 16(b) $\boldsymbol{i e}=\mathbf{0 . 0 0} ; \boldsymbol{i c}=\mathbf{0 . 0 0} ; \boldsymbol{g}=\mathbf{1 . 0 0} ; \boldsymbol{i f}=\mathbf{0}: 00$ Pure Outgoing Scenario 11

| $P$ | $R T T$ | \% increase | $H C$ | \% increase | MTT (up- <br> down ave) | \% increase | $H$ |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 10 | 120.842 | 0.000 | 10.000 | 0.000 | 56.221 | 0.000 | 0.083 |
| 12 | 118.377 | -2.040 | 10.000 | 0.000 | 56.200 | -0.037 | 0.084 |
| 16 | 113.370 | -6.183 | 10.000 | 0.000 | 55.231 | -1.761 | 0.088 |
| 20 | 109.456 | -9.422 | 10.000 | 0.000 | 54.250 | -3.506 | 0.091 |
| 30 | 102.894 | -14.852 | 10.000 | 0.000 | 52.370 | -6.850 | 0.097 |
| 40 | 98.976 | -18.095 | 10.000 | 0.000 | 51.158 | -9.006 | 0.101 |

Table 17(a) $i e=0.00 ; i c=0.00 ; g=0.00 ; i f=1.00$ Pure Interfloor Scenario 12

| \# of passengers demanding <br> service around the building | 10 <br> $(C C)$ | 12 <br> $(1.2 C C)$ | 16 <br> $(1.6 C C)$ | 20 <br> $(2 C C)$ | 30 <br> $(3 C C)$ | 40 <br> $(4 C C)$ |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: |
| \# of up-stops | 5.894 | 6.388 | 7.057 | 7.443 | 7.793 | 7.787 |
| \# of down-stops | 5.896 | 6.387 | 7.035 | 7.443 | 7.792 | 7.787 |
| Highest floor reached | 10.941 | 10.967 | 10.982 | 10.997 | 11.000 | 11.000 |
| Lowest floor reached | 4.058 | 4.032 | 4.010 | 4.003 | 4.000 | 4.000 |
| \# of up-passengers | 5.0 | 6.0 | 8.0 | 10.0 | 14.3 | 16.9 |
| \# of down-passengers | 5.0 | 6.0 | 8.0 | 10.0 | 14.3 | 16.9 |
| \% of up-coincidental floors | 0.566 | 0.652 | 0.782 | 0.866 | 0.962 | 0.987 |
| \% of down-coincidental floors | 0.566 | 0.651 | 0.782 | 0.869 | 0.962 | 0.987 |
| Round trip time (s) | 122.934 | 133.403 | 150.383 | 163.949 | 187.941 | 200.277 |
| Average up-transit time (s) | 27.049 | 28.979 | 32.097 | 34.556 | 38.858 | 40.910 |
| Average down-transit time (s) | 27.058 | 28.966 | 32.083 | 34.571 | 38.861 | 40.900 |

Table 17(b) $\boldsymbol{i e}=\mathbf{0 . 0 0} ; \boldsymbol{i c}=\mathbf{0 . 0 0} ; \boldsymbol{o g}=\mathbf{0 . 0 0} ; \boldsymbol{i f}=\mathbf{1 . 0 0}$ Pure Interfloor Scenario 12

| $P$ | $R T T$ | \% increase | $H C$ | \% increase | $M T T$ (up- <br> down ave) | \% increase | $H C / R T T$ |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 10 | 122.934 | 0.000 | 10.000 | 0.000 | 27.054 | 0.000 | 0.081 |
| 12 | 133.403 | 8.516 | 12.000 | 20.000 | 28.973 | 7.093 | 0.090 |


| 16 | 150.383 | 22.328 | 16.000 | 60.000 | 32.090 | 18.617 | 0.106 |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| 20 | 163.949 | 33.363 | 20.000 | 100.000 | 34.564 | 27.760 | 0.122 |
| 30 | 187.941 | 52.880 | 28.600 | 186.000 | 38.860 | 43.639 | 0.152 |
| 40 | 200.277 | 62.914 | 33.800 | 238.000 | 40.905 | 51.200 | 0.169 |

## 4 OBSERVATIONS AND ANALYSIS

## Observations on Raw Data

It can be seen from most tables (a), e.g. Tables 11(a) and 17(a) etc., that the number of up-stops and number of down-stops keep on increasing as $P$ is increasing in general, with three exceptions. Such an increase is reasonable because the main idea of this and the previous article (So et al. 2022b) states that a passenger demand of $P \leq C C$ in fact has not fully utilized the design capacity of the system. Such conclusion can also be arrived later when $H C$ and $H C / R T T$ are analyzed.

For those pure incoming (Table 15(a)) or pure outgoing (Table 16(a)), either one can always be zero because either type of traffic actually does not exist. Also, for these extreme cases, the number of upor down-stops starts to decrease right from the beginning when $P$ begins to go beyond $C C$. This is because the chance of more passengers who want to go to the same destination floor increases.

In general, the number of up- and/or down-stops start(s) to decrease as $P$ approaches $4 C C$. This is reasonable as the demand far exceeds the design capacity while the system has been driven to saturation.

For normal uppeak (Table 6(a)) and normal down peak (Table 7(a)) conditions, it can be seen that the number of stops of opposite direction of travel, i.e. down-stops under uppeak and vice versa, keeps on increasing even until $P=4 C C$. This is because one round trip must be considered as two separate journeys, i.e. the up-journey and the down-journey. The reason why the number of down-stops can continue to increase under an uppeak condition, and vice versa, is that the design capacity actually has not been fully utilized in the opposite direction.

Next, the highest and lowest floors reached are considered. Except pure interfloor (Table 17(a)), for all scenarios, the highest floor reached gradually approaches the top floor, i.e. 11th floor, and the lowest floor reached gradually approaches the bottom floor, i.e. 1st floor, as $P$ is increasing. Even under a pure interfloor condition, the highest floor reached approaches the top floor while the lowest floor reached approaches the 4th floor which is the bottom floor of the occupant floor zone. This is obvious because as $P$ is getting larger, the chance of origin and destination floors taking all floors of the whole building is getting higher and higher.

Finally, the proportion, indicated by symbol \% between 0.0 and 1.0 , of up-coincidental floors and down-coincidental floors is considered. As $P$ is getting larger, it can be seen that the proportion is approaching unity. The exact definition of the proportion of up-coincidental floors here means the percentage (between 0.0 and 1.0) of trials out of 500,000 where the first stop of an up-journey coincides with the last stop of a down-journey and this equally applies to the number of downcoincidental floors. As the demand, $P$, is increasing, more and more passengers enter the building at the 1st floor and exit there, as well as traveling to the top floor and entering the elevator at the top floor. Furthermore, the chance of up-coincidental floors is usually higher than that of downcoincidental floors, which is reasonable as the main terminal is supposed to be the busiest floor throughout the whole building.

## Observations on Processed Data

Here, three important processed parameters are analyzed.
The $R T T$ has a huge impact on system design. Throughout the decades, designers have been desiring to shorten the $R T T$ of the round trip because $R T T$ relates to the interval which is also related to the $A W T$ of passengers. Therefore, $R T T$ is the true indicator of the quality of service.

Second, the $H C$ is important because this relates to the exact number of passengers that can be handled, which is related to the quantity of service. Readers are reminded that the definition of $H C$ in this article is different from the conventional one which is the number of passengers that can be handled in a 5 -minute interval. Here, the $H C$ means the number of passengers that can be handled by one elevator within one round trip. In other words, a slightly longer $R T T$ is worth considering provided that the $H C$ is increasing by a certain level. Hence, the ratio $H C / R T T$ is important, the higher the better, meaning that more output can be obtained with less input. This is somehow analogue to the concept of COP (coefficient of performance) in the HVAC (heating, ventilating and air-conditioning) industry. Even if more electrical energy is consumed by a chiller, it is worth it if the amount of heat removed by the chiller is also increased by a greater amount.

Finally, the MTT (mean transit time) is important as it indicates the average time when a passenger needs to spend inside an elevator on his/her way to the destination. In some way, the MTT together with the $A W T$ represent the quality of service.

Figure 1 shows the variation of $R T T$ against $P$ under all 12 scenarios. It can be seen that in general, the $R T T$ curve rises initially until it approaches $P=4 C C$. There are exceptions here. As explained in the last section, for CIBSE Office uppeak or CIBSE Office down peak conditions, the number of stops can continue to increase in either travel direction opposite to that of the peak condition. Under this situation, there is room for further increase in the RTT because not the full design capacity of the opposite travel direction has been utilized even when $P=4 C C$. Such performance can also be seen during a weak uppeak or weak down peak condition.

Figure 2 shows the variation of $H C$ against $P$ under all 12 scenarios. It can be seen that under all conditions, the $H C$ keeps on increasing as $P$ is increasing except the pure incoming, i.e. uppeak, and pure outgoing, i.e. down peak, conditions because the $H C$ keeps constant as explained earlier. In other words, in general, the system always has some room for taking up more passengers when $P>C C$. In particular, during the two lunch peaks, mixed and pure interfloor conditions, $H C$ can catch up with $P$ up to $P=2 C C$. This is very encouraging. The system can handle more passengers when a more balanced up- and down- traffic conditions exist.


Figure 1 Round Trip Time against Passenger Demand under 12 scenarios


Figure 2 Handling Capacity against Passenger Demand under 12 scenarios

Whether a higher $H C$ is really desirable or not very much depends on the cost of it, i.e. the RTT. Figure 3 shows the variation of $H C / R T T$ against $P$. It can be seen that for most scenarios, except the pure incoming, i.e. uppeak, scenario, the curve is rising as $P$ is increasing. That is desirable as the output, i.e. $H C$, is improving whereas the input, $R T T$, is not increasing by the same amount. The parameter, $H C / R T T$ should be as high as possible. It seems that it is rather easy for a system to be saturated under a pure uppeak condition. That may explain why over the past decades, designers have been focusing on uppeak conditions only. First, it is mathematically easier to work on uppeak traffic. Second, it may be the worst case to consider. More discussion can be found in Chapter 13 of (Barney
et. al. 2016). If the system is well designed to handle uppeak, it could be able to handle other traffic conditions more satisfactorily. Having said that, the ratio, $H C / R T T$ still rises when $P$ does not go beyond $C C$ by too much, i.e. $P \leq 2 C C$. With a view to the recent belief of the industry that pure incoming or uppeak is rare, the conventional design rules may oversize the system.


Figure 3 The ratio of $\boldsymbol{H C}$ over $\boldsymbol{R T T}$ against Passenger Demand under 12 scenarios


Figure 4 Mean Transit Time against Passenger Demand under 12 scenarios

The champion goes to Scenario 12, pure interfloor traffic, where the ratio is highest even when $P=4$ $C C$. First, the travel distance of the elevator is shorter during pure interfloor because the lift basically serves the occupant floor zone only, not the entire building. Second, there is a more or less balanced
up- and down- traffic during such pure interfloor condition. However, the risk is that pure interfloor may consist of sub-uppeak or sub-down-peak conditions. Under such sub-conditions, the ratio may not be that high and the two curves of the two lunch peaks, i.e. Scenarios 3 and 4, should be referred to.

Finally, the second parameter indicating the quality of service other than the $A W T$ is considered. Figure 4 shows the variation of $M T T$ against $P$. It can be seen from the left chart that the curves of the two lunch peaks keep on rising until saturation, which is not a desirable phenomenon. This behaviour can also be noticed for the mixed, weak uppeak and weak down peak conditions. That implies although a more or less balanced up- and down- traffic can boost $H C$, the cost is an increase in $M T T$ where passengers need to spend more time in the elevator on average. Having said that, even when $P$ has grown from 10 to 20, i.e. an increase by $100 \%$, the $M T T$ has not grown by the same ratio. Under normal and extreme uppeak and down peak conditions, the $M T T$ starts to decrease as $P$ is increasing.

It is interesting to note that as $P$ is getting larger and larger, both $R T T$ and $M T T$ tend to get saturated. But $H C$ can further increase, though with a much lower rate as compared with that when $P$ is small. That explains why $H C / R T T$ can slightly increase even when $P$ is approaching 40 , four times the $C C$. The reason is that the exact $H C$ that one elevator can provide within one round trip very much depends on the distribution of the landing and car calls around the building, not only on $P$, as illustrated by Table 1. If most car calls are short trips and landing calls widely distributed, say from $1 / \mathrm{F}$ to $4 / \mathrm{F}$, from $4 / \mathrm{F}$ to $5 / \mathrm{F}$, from $5 / \mathrm{F}$ to $6 / \mathrm{F}$, and so on, the $H C$ could be rather high. Hence, though the $H C$ may get saturated for some cases, there is room for growth for other cases, which may explain why on average, $H C$ can continue to rise, but gradually slower and slower. In practice, usually, there is more than one elevator in one bank while the supervisory control can balance the dispatching of different elevators to serve different landing calls.

## 5 CONCLUSIONS

It is conventional that system design of the elevator industry starts with a traffic analysis on pure incoming traffic patterns during the uppeak period by calculation to estimate the round trip time ( $R T T$ ), 5 -minute handling capacity (HC), uppeak interval (UPPINT), average waiting time (AWT), and average transit time ( $A T T$ ) respectively. This process is followed by in-depth real time computer simulation on selected scenarios to arrive at the final design, as recommended by ISO 8100-32: 2020 for office, hotel and residential buildings. Over the past two decades, it has been found that pure incoming traffic is no longer the dominant traffic pattern of a modern office building and a typical one consists of a mixture of incoming, outgoing and interfloor modes. That led to the development of the universal traffic analysis approach by working on an origin-destination matrix where the Universal RTT and HC etc. are computed.

Under a pure incoming traffic condition, the total demand $(P)$ of one round trip of an elevator cannot go beyond the contract capacity $(C C)$ as conventionally assumed. Based on the proposed theoretical concept of a previous study and the in-depth simulation results of this article, it is shown that a system usually has room for handling more passengers for $P$ to go beyond $C C$, in particular, during a downjourney of an uppeak condition or the up-journey of a down peak condition. In other words, the system has potential to increase $H C$ during a journey opposite to the current traffic mode.

By this argument, it is shown by simulation that during a more or less balanced up- and down-traffic mode, $H C$ can easily approach $P=2 C C$. Having said that, under most conditions, $P$ can easily go beyond $C C$ except under a pure incoming or pure outgoing traffic mode. It is also shown in this article that $H C$ accomplishment is more constrained under a pure incoming mode. And that may explain why over the decades, pure incoming traffic has been the focus of designers because it may be the worst case to handle, and the safety margin of design is higher. If the system is well designed to accommodate pure incoming traffic, it may be able to handle other traffic patterns. But if the safety margin is always higher, the system may be oversized, thus wasting resources. Having said that, lunch peaks may consist of heavy incoming and outgoing passengers and these could be the critical headache.

The parameter, $H C / R T T$, was proposed to indicate whether the number of passengers handled could be increased by keeping a relatively shorter round trip time. And it is found that pure interfloor traffic, without any incoming or outgoing passengers, favours a higher $H C / R T T$ when $P$ is getting higher. Having said that, though a more balanced up- and down- traffic can boost $H C$, the cost is an increasing mean transit time (MTT).

Therefore, an optimal system design needs to consider a compromise between short RTT, short interval (INT), short $A W T$, high $H C$ and short $M T T$. It seems that such optimal design may make use of the small range from $P>C C$ until $P \leq 2 C C$. At this moment, there is no formula in the world that allows all these be analytically studied by calculation. And if real time dispatcher-based computer simulation is to be carried out, a consideration of so many different cases may imply a very intensive computational load. Therefore, Monte Carlo simulation using the PDFOD and CDFOD matrices may provide a balanced solution between the two, demonstrating the usefulness of Monte Carlo simulation in system design. Moreover, it is shown in this article that the total passenger demand, rather than a probability distribution function alone adopted in the traditional RTT calculation, needs to be an important input element to the calculation that can easily be applied by practitioners. In other words, this approach may allow Monte Carlo simulation to be easily incorporated into popular traffic analysis software using the same inputs as other techniques, while the results could be cross compared with those obtained by dispatcher-based simulations [19].

Furthermore, although $H C$ may give some indication of the performance of the overall elevator service, $A W T$, the average waiting time of passengers, should be another which may perhaps be more important. $A W T$ obviously tends to increase significantly when $P$ is getting larger. And this could be a further study consequent to what has been reported in this article.

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